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Urban Perspectives Ltd PO Box 9042 Marion Square **Wellington 6141**

TDG Ref: 12834.001 27 February 2015

Issued via email: <u>alistair@urbanp.co.nz</u>

Attention: Alistair Aburn

Dear Alistair

North Kumutoto Precinct Project Response to WCC Request for Further Information

Council's Request dated 5 February 2015 seeks further information and clarification on a number of urban design, traffic and related matters.

Items 10 through 24 relate to Traffic and Parking, each of which were discussed with Council's transport network manager, Mr Soon Kong, on 10 February. This response has been informed by discussions at that meeting.

This report addresses each item in turn, and is supported by accompanying plans. For ease of reference, the same numbering convention is used.

10 Please provide full details of the intersections (and approaches) and the pedestrian crossing facilities across Customhouse Quay, north of Whitmore Street. These details should include lane widths, dimensions and turning paths and other relevant details which assist in their operation.

Appendix A includes a scaled plan with dimensions (refer Drawing number 1.045 prepared by Isthmus).

Appendix A also includes a separate plan illustrating the tracking paths of a standard 8m truck, as defined by the District Plan, turning to and from Customhouse Quay (refer Figure 8 prepared by TDG).

11. Please clarify whether the new footpath to be provided alongside Site 9 (between the Whitmore Street gates and Waring Taylor Street) will be within legal road or within a private site (please indicate the site boundary of the proposed plan).

Appendix B includes two plans with dimensions showing the intended footpath arrangements along Customhouse Quay, and also showing the property boundary (refer Drawing Numbers 1.044 and 1.046 prepared by Isthmus).

As confirmed at the 10 February meeting, the proposed arrangements do not intend any changes to the existing kerblines of Customhouse Quay past sites 9 and 10, except where required to form the new Whitmore Street entrance.



12. Please provide details of the proposed modifications to the traffic lanes along Customhouse Quay (see Figure 3 of the Traffic Report by TDG). This should include the lane width(s), footpath width, truck turning paths and other relevant details which assist in its function.

Figure 3 of TDG's September 2014 Transportation Assessment Report included duplicate lane markings on Customhouse Quay. The proposal does not intend any changes to the existing traffic lanes and markings, and Figure 3 has been cleaned and a fresh drawing included in Appendix C.

13. Please provide Traffic Engineering advice on how pedestrian safety (and that of other users) will be maintained through the use of the 'shared space'. Please explain how speed will be controlled, detail any distinguishing features (surface treatment, speedbumps etc).

The new Kumutoto laneway is proposed with treatments and outcomes consistent with the existing southern portion of the laneway, including raised platforms to define the Whitmore Plaza and the Wool Store Plaza, and banded areas of asphalt and concrete paving.

The same principles of shared spaces that exist in Kumutoto Lane (south) and elsewhere on the waterfront are proposed in this instance.

The concept is well established. There are numerous situations where pedestrians co-exist with vehicles, without the need to demarcate space for different users.

As illustrated by the series of photographs below, there are examples alongside Shed 6, at the Brandon Street access to the TSB Arena carpark, and around Herd Street, including the similar ramp connections to the basement carparks servicing the Chaffers Dock Apartments and the Clyde Quay Wharf Apartments where pedestrians and vehicles currently share the space safely.



Lane alongside Shed 6



Brandon Street shared area







Clyde Quay Wharf shared area

Herd Street shared area

For the most part, and as proposed for North Kumutoto, these areas use variations in paving and/or street furniture, rather than traditional traffic signs and markings, to provide sufficient cues to pedestrians and drivers, while maintaining a predominantly pedestrian environment.

Vehicle speeds will be slow, and with low vehicle volumes, priority can be shared and users can make way for one another, in the manner illustrated by these examples.

14. Please provide details of the input data, phase timing and output etc, used for the traffic modelling presented. Council Traffic Advisors wish to review this material.

A summary of the performance of the existing and changed Whitmore Street intersection is included at Tables 5 and 6 of the September 2014 Transportation Assessment Report, for the two-way and one-way lane configurations respectively. Six scenarios are included in each instance, covering the AM, PM and Saturday peaks and the existing (Ex) and future (Fut) configurations.

Appendix D1 includes summaries of the SIDRA data for the two-way lane configuration.

Appendix D2 includes scenarios of the SIDRA data for the one-way lane configuration.

15. Please provide details of how any parallel movements from the adjoining Centreport Land will interact with the new shared access lane.

There is no intention to provide two parallel roadways to the rear of Shed 21 and Site 10. Rather, the existing laneway will shift westwards to the positions shown on the application plans, and the existing laneway space within Centreport land will be demarcated from the new Kumutoto Lane with timber beams, and available for pedestrians and cyclists.

The proposed arrangements are shown by the cross-sections included in Appendix E (refer Drawing Number 2.056 prepared by Isthmus).

16. Please provide details of the altered car park layout for Site 9 (including any subsequent hard/soft landscaping changes).

Drawing Number 1.046 prepared by Isthmus and included in Appendix B is a scaled plan with dimensions showing the carpark layout, including a stall depth of 4.4m, an overhang of 0.65m and an aisle width of 6.2m.



17. Please explain what measures will be implemented to ensure that vehicles exiting the parking ramp will not compromise public safety. These could include measures to warn pedestrians along the building edge of exiting vehicles (via an audible and/or visual system), as well as signal controls for users of the one-way ramp for entry and exit.

Note: Council's Traffic Advisor has suggested that speed bumps should be installed near the exit of the commercial building to ensure that this is a low-speed environment.

Following the 10 February meeting, a careful review has been undertaken of the carpark ramp, and an updated design developed that presents a safer interface with the Wool Store Plaza.

The developed design incorporates:

- sight triangles in the manner anticipated by the District Plan, presenting required intervisibility between exiting drivers and pedestrians;
- a flat (1:20) grade at the top of the ramp on which vehicles can wait momentarily before exiting the building, should drivers need to yield to pedestrians;
- a roller door that will function as a control point, with an audible sound when it opens and closes that will heighten the awareness of users in the area;
- a judder bar positioned just inside the roller door, that will present a slow control point for vehicles before exiting onto the Plaza space;
- an external electronic 'Car Coming' sign that will alert users of the Plaza when cars exit;
 and
- traffic signals to control inbound and outbound movements on the single width ramp.
 These signals will rest in green for inbound vehicles.

These intended arrangements are very similar to the carpark ramp design at One Market Lane, as illustrated in the photo below, except that in that instance the ramp accesses the floors above.



Appendix F includes the relevant plans (refer SK_06-C and SK_05-D prepared by Athfield Architects).

Also included in Appendix F is a revised layout for the basement carpark (refer SK_02-D prepared by Athfield Architects). This revised layout avoids the previous awkward



arrangement of tandem carparks and presents a total of 62 parking spaces, being four less than the previously – proposed total of 66 spaces.

18. Please provide tracking paths for larger service vehicles (semi-trailer and a large rigid truck) turning into and out of the intersection with the narrowing of the entry and exit at Customhouse Quay.

As confirmed at the 10 February meeting, the area of North Kumutoto and its activities and buildings do not attract articulated trucks. Rather a standard 8m truck, as defined by the District Plan, is the appropriate design vehicle.

Such a truck is suitably representative of a standard 7.7m Type 2 Medium Pumper fire appliance and a 8.0m Type 3 Heavy Pumper fire appliance.

The tracking paths for an 8m standard truck turning into and out of the intersection were included earlier in response to Item 10.

19. Please provide details of how the internal roading network is to be controlled, including interactions with users of Site 9.

The intended arrangements are described above in response to Item 13.

20. Please provide details of the width of the proposed public footpath adjoining Site 10.

Appendix B, as described previously, includes the relevant plan confirming the proposed footpath widths.

21. Please provide dimensions of the types of vehicles servicing this development (eg rubbish trucks, furniture removal). Please clarify whether all tenancies will have access to the servicing area and how any shared arrangement will be managed. Are there other servicing areas publicly available as an alternative space if the internal loading area is occupied?

Note: It is likely that any service vehicle parked adjacent to the building will block the access lane and therefore, all servicing must be undertaken on-site.

Following the 10 February meeting, further consideration has been given to the design of the loading bay and the intended loading arrangements. With an available headroom of 3.34m, the internal loading bay will mostly suit cars, vans and small rigid trucks. Larger vehicles will use the inset bays within the laneway and a kerbside zone will be allocated for this purpose.

The arrangements will be very similar to the established loading practices associated with the Meridian Building.

The most frequent visits by larger trucks will be for the collection of waste. In the same manner as the Meridian Building, rubbish removal will be contracted to occur during 'midnight' hours.

Following the same principles as for the carpark ramp, the loading bay itself has been redesigned to add sight triangles in the manner shown by SK_06-C included in Appendix F.

A service corridor extends from the rear of the loading bay to provide direct access to the central lift core and the majority of tenancies. Other tenancies will be accessed from around the perimeter of the building.

22. Please provide details on how users of the service dock will enter from, and exit onto the shared access lane safely (including tracking curves).

The manoeuvres of a truck turning to and from the laneway (in both its two-way and one-way form) were illustrated by Figure 7 included in September 2014 Transportation Assessment Report. That diagram has been updated to reflect the new arrangements, and included as Figure 7A in Appendix G.

The arrangements show that driveway design changes will be needed in the event that a one-way lane is constructed.

23. Please provide details of the proposed gradient(s) into the basement level.

SK_05-D included earlier at Appendix F shows the updated carpark ramp, which has been designed with the following grades:

- a 1:8 transition from the basement carpark;
- a 1:4 central length;
- a 1:8 transition towards the top of the ramp; and
- **a** 1:20 flat section at the top in advance of vehicles exiting onto the Wool Store Plaza.

By way of example, the same grades exist on the carpark ramp for One Market Lane, except in that instance the flatter section at the bottom of the ramp on the approach to the footpath is graded at 1:12.

24. Please provide details of how all required Emergency Service Vehicles will be able to continue using shared space (where required).

With the laneway proposed to be designed with the same form as the existing southern laneway, as described earlier in response to Item 13, emergency services will be able to use the new northern laneway in the same manner.

Fire appliances will be able to access and egress the area via the new Whitmore Street entrance in the manner shown previously by the vehicle tracking diagrams included in Appendix A.

We trust this response and accompanying plans fully addresses the traffic and parking matters raised in Items 10 through 24.

Yours sincerely

Traffic Design Group Ltd

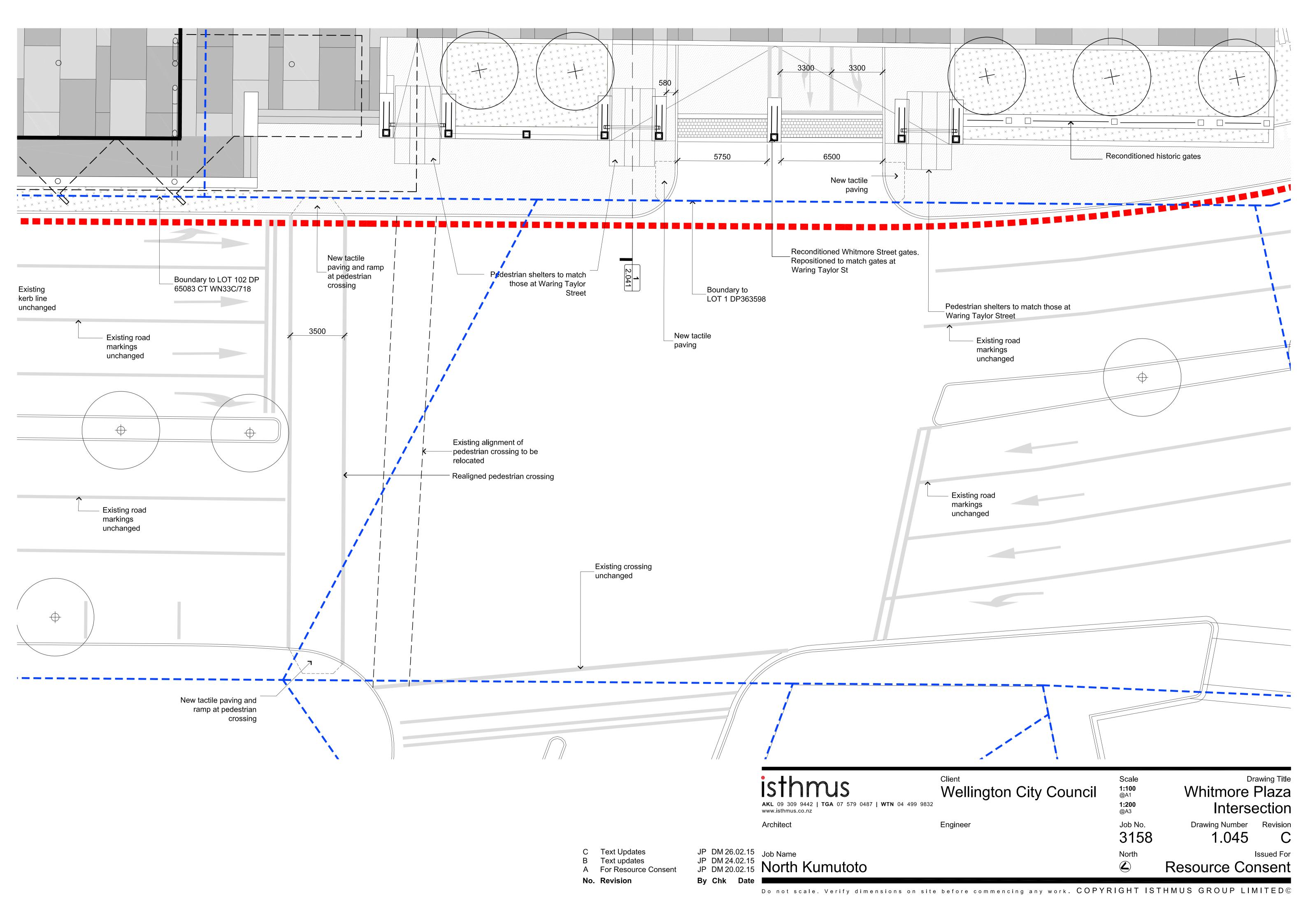
Mark Georgeson

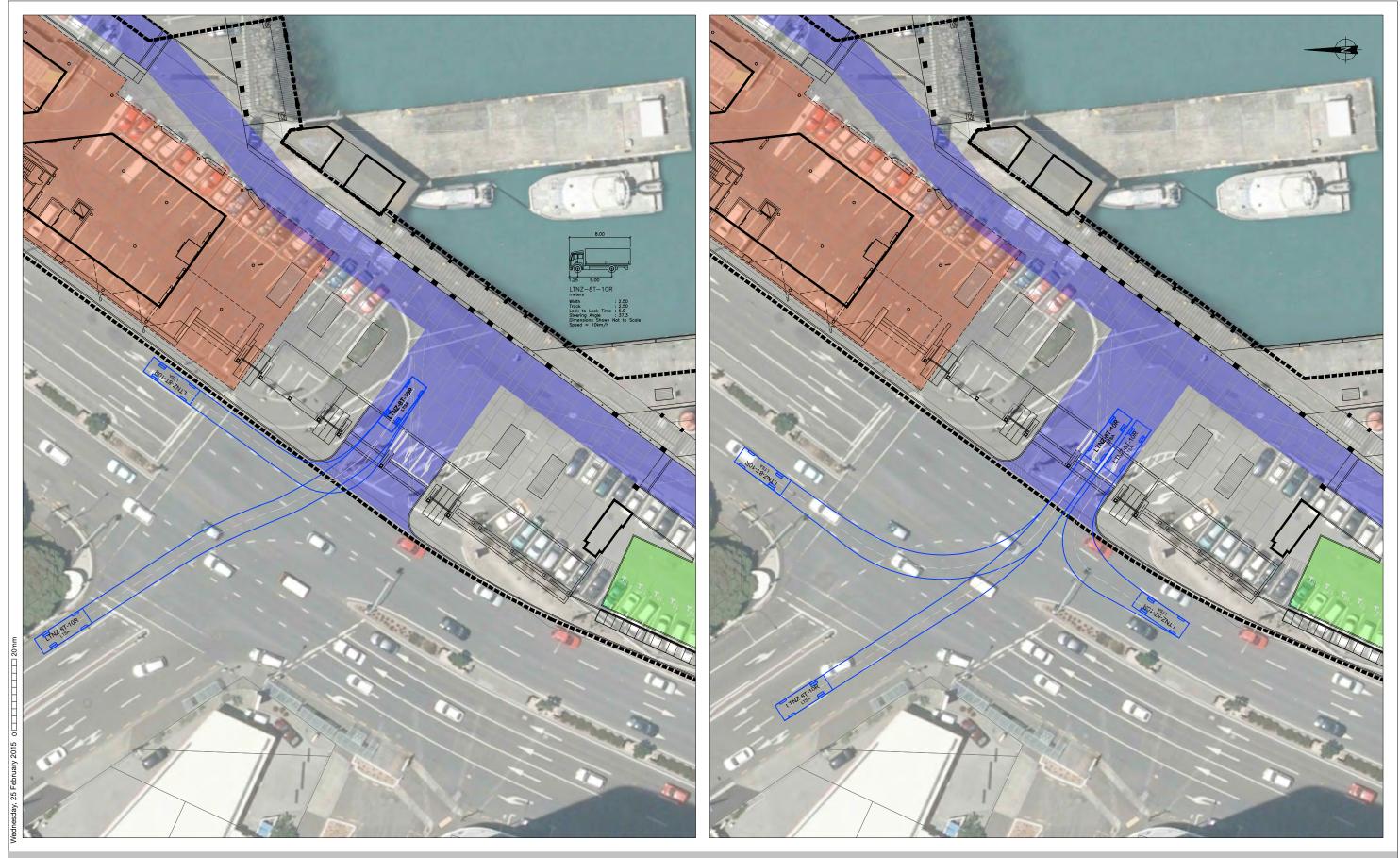
Director

mark.georges on @tdg.co.nz

Appendix A

Plans Responding to Item 10





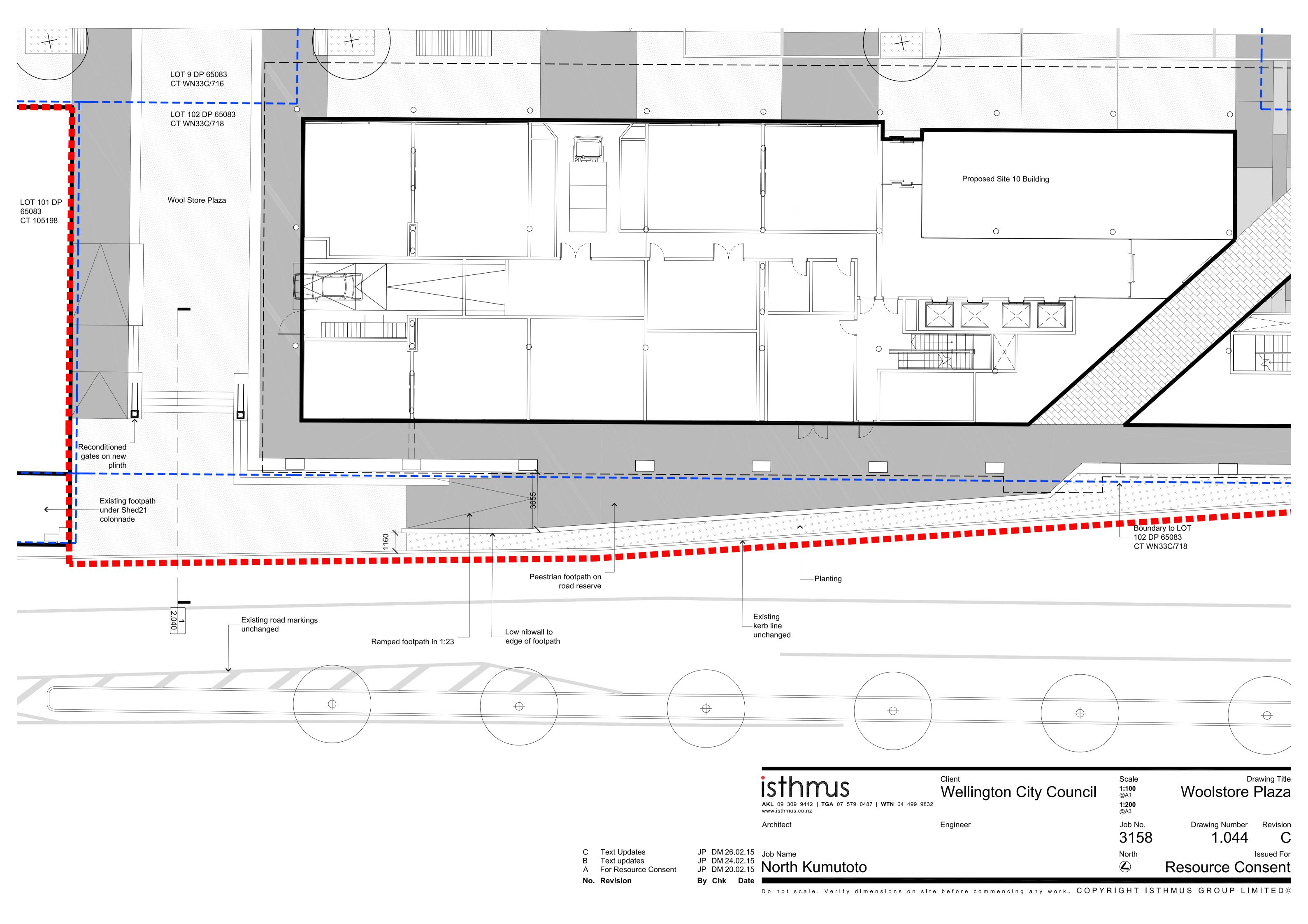
REVISION	DATE	DESCRIPTION

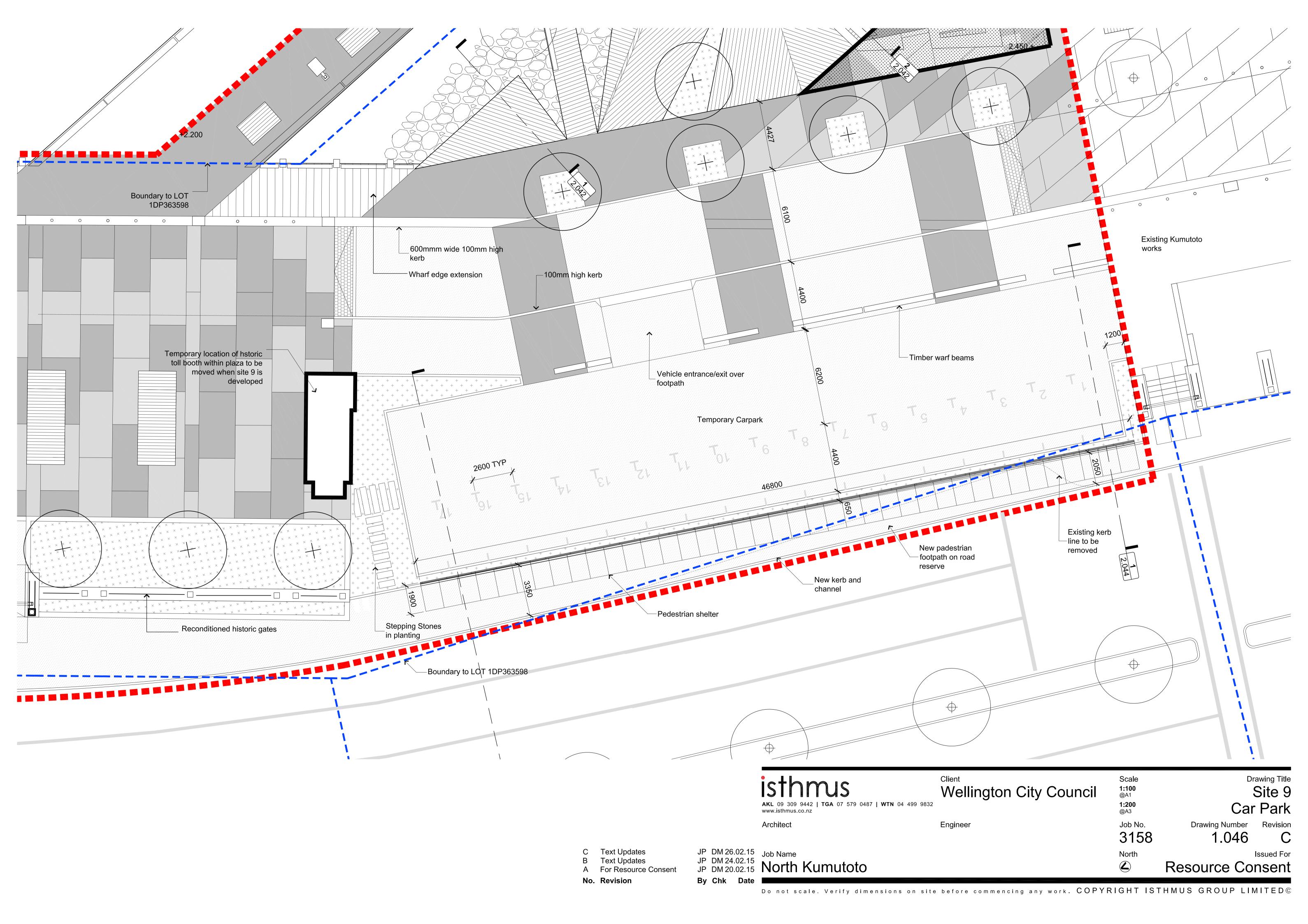
Kumutoto Precinct: Site 10 and Open Space Development Intersection Tracking for Medium Rigid Truck DRAWN: Quentin O'S
DATE: 25/02/2015
SCALE: 1:500 @ A3
DWG NO:12834W1A



Appendix B

Plans Responding to Item 11





Appendix C

Plan Responding to Item 12



REVISION	DATE	DESCRIPTION

Kumutoto Precinct: Site 10 and Open Space Development

Proposed Site Layout

DRAWN: Quentin O'S
DATE: 25/02/2015
SCALE: 1:1000 @ A3
DWG NO:12834W1A



Appendix D1

Data Responding to Item 14 (Two-Way Lane Configuration)

Site: 12834 Whitmore St Ex AM

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Mov	OD	Demand	Flows	Deg.	Average	Level of	95% Back (Prop	Effective	Average
ID)	Mov	Total	HV %	Sath	Delay	Service	Vehicles veh	Distance m	Quetied	Stop Rate per veh	Speed km/l
South:	Customhou	veh/h se Quav	year and the second	V/c	Sé¢						
1	L2	582	2.0	0.886	42.8	LOS D	28.8	205.1	1.00	0.93	34.0
2	T1	1083	2.0	0.664	30.0	LOS C	15.1	107.8	0.94	0.81	40.
Appro	ach	1665	2.0	0.886	34.5	LOS C	28.8	205.1	0.96	0.85	38.
East: \	∕WL										4.400.000
4	L2	14	0.0	0.081	47.6	LOS D	0.5	3.3	0.96	0.67	33.
5	T1	19	0.0	0.081	42.0	LOS D	0.5	3,4	0.96	0.65	35.4
6	R2	12	0.0	0.088	47.7	LOS D	0.5	3.5	0.96	0.67	33.
Appro	ach	44	0.0	0.088	45.2	LOS D	0.5	3.5	0.96	0,66	34.
North:	Waterloo Qu	uay									
7	L2	105	2.0	0.889	42.5	LOS D	29.3	208.4	1.00	0.95	36.
8	T1	1699	2.0	0.889	36.9	LOS D	29.5	209.7	1.00	0.95	37.
9	R2	66	2.0	0.880	106.0	LOS F	6.1	43.7	1.00	0.92	21.
Appro	ach	1871	2.0	0.889	39.7	LOS D	29.5	209.7	1.00	0.95	36.
West:	Whitmore S										
10	L2	86	2.0	0.341	27.2	LOS C	7.3	52.2	0,77	0.75	41.
11	T1	53	2.0	0.341	21.6	LOS C	7.3	52.2	0.77	0.75	42.
12	R2	312	2.0	0.341	27.3	LOS C	7.3	52.2	0.77	0.77	41.
Аррго	ach	451	2.0	0.341	26.6	LOS C	7.3	52.2	0.77	0.76	41.
110000	hicles	4031	2.0	0.889	36.1	LOS D	29.5	209.7	0.96	0.88	37,

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Move Mov JD	ment Performance - Pedestria Description	ns Demand Flow ped/h	Average Delay	Level of Service	Average Back o Padestrian ped	of Queue Distance m	Prop. Queued	Effective Stop Rate per ped
P3	North Full Crossing	53	32.8	LOS D	0.1	0.1	0.88	0.88
P4	West Full Crossing	53	34.4	LOS D	0.1	0.1	0.90	0.90
All Pe	destrians	105	33.6	LOS D			0.89	0.89

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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SIDRA INTERSECTION 6

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Site: 12834 Whitmore St Ex PM

New Site

Signals - Fixed Time Cycle Time = 160 seconds (Practical Cycle Time)

Mov	OD	Demand		Deg.	Average	Level of	95% Back		Prop.	Effective	Averag
ID)	Mov	Total veh/h	HV %	Saln V/c	Delay sec	Service	Vehicles veh	Distance m	Queued	Stop Rate per veh	Speed km/
South	: Customhou										
1	L2	525	2.0	0.866	41.0	LOS D	25.8	184.0	1.00	0.92	35.
2	T1	1211	2.0	0.799	33.3	LOS C	18.1	129.2	0.99	0.88	38.
Appro	ach	1736	2.0	0.866	35.6	LOS D	25.8	184.0	1.00	0.89	37.
East:	WWL				Altanience Wither						
4	L2	48	0.0	0.207	46.1	LOS D	1.3	9.0	0.97	0.71	33.
5	T1	40	0.0	0.207	40.5	LOS D	1.3	9.3	0.97	0.70	35.
6	R2	40	0.0	0.287	46.6	LOS D	1.8	12.4	0.98	0.73	33.
Appro	ach	128	0.0	0.287	44.5	LOS D	1.8	12.4	0.97	0.71	34.
North	Waterloo Q	uay							6 () = 0 () 6 () may 6 () 1 ()		
7	L2	42	2.0	0.753	29.7	LOSC	18.8	134.0	0.94	0.83	41.
8	T1	1512	2.0	0.753	23.8	LOS C	18.9	134.5	0.93	0.81	43.
9	R2	108	2.0	0.861	95.6	LOS F	9.3	66.1	1.00	0.92	23.
Appro	ach	1662	2.0	0.861	28.7	LOS C	18.9	134.5	0.93	0.82	40.
West:	Whitmore S	t arahan kan						Zurkanasti.			Any views:
10	L2	343	2.0	0.632	30.9	LOSC	15.0	106.5	0.90	0.83	39
11	T1	42	2.0	0.632	25.3	LOS C	15.0	106.5	0.90	0.83	40
12	R2	126	2.0	0.208	27.0	LOS C	4.1	29.4	0.76	0.74	41
Appro	ach	512	2.0	0.632	29.5	LOS C	15.0	106.5	0.87	0.81	39.
Λ II \	hicles	4038	1.9	0.866	32.3	LOS C	25.8	184.0	0.95	0.85	39

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Mov	ment Performance - Pedestr Description	Demand Flow	Average Delav		erage Back of ledestrian	Queue Distance	Prop. Queued	JEffectiv Stop Ra
U		ped/h	8é¢		presel	m	0.00]ଶ୍ୟାଣ୍ଡ 0.9
93	North Full Crossing	53	34.3	LOS D	0.1	0.1	0.92 0.93	0.9
74	West Full Crossing	53	34.8	LOS D	U.1	U, 1 777-11: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1:		UERIA E E E

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Site: 12834 Whitmore St Ex Sat

New Site

Mov	ØĐ	Demand	Flows	Deg.	Average	Level of	95% Back		Prop	Effective	Average
ID	Mov	Total veh/h	HV %	Satn V/c	Delay sec	Service	Vehicles veh	Distance m	Queued	Stop Rate per veh	Speed km/h
South:	Customhou	A SECULIAR S									
1	L2	506	2.0	0.871	43.4	LOS D	24.7	176.1	1.00	0.92	34.5
2	T 1	1576	2.0	0.910	46.3	LOS D	30.2	215.2	1.00	0.99	34.2
Approa	ach	2082	2.0	0.910	45.6	LOS D	30.2	215.2	1.00	0.97	34.2
East; V	VVVL										
4	L2	40	0.0	0.153	48.2	LOS D	0.9	6.2	0.97	0.70	33.0
5	T1	17	0.0	0.122	42.3	LOS D	0.7	5.2	0.97	0.67	35.6
6	R2	11	0.0	0.080	47.7	LOS D	0.5	3.2	0.96	0.67	33.3
Appro	ach	67	0.0	0.153	46.6	LOS D	0.9	6.2	0.97	0.69	33.7
North:	Waterloo Q	uay		ÇUR KÜNE		7-18 19-10 19-10 17-17-18-18					
7	L2	52	2.0	0.667	28.2	LOS C	17.9	127.1	0.88	0.78	42.6
8	T1	1448	2.0	0.667	22.4	LOSC	17.9	127.7	0.87	0.77	43.8
9	R2	105	2.0	0.888	103.8	LOS F	9.7	69.1	1.00	0.94	22.0
Appro	ach	1605	2.0	0.888	27.9	LOS C	17.9	127.7	0.88	0.78	41.1
West:	Whitmore S	t in the second									
10	L2	185	2.0	0.336	29.7	LOS C	6.7	47.6	0.81	0.78	39.7
11	T1	11	2.0	0.336	24.2	LOS C	6.7	47.6	0.81	0.78	40.5
12	R2	25	2.0	0.043	27.2	LOS C	8,0	5.5	0.72	0.68	41.
Appro	ach	221	2.0	0.336	29.2	LOSC	6.7	47.6	0.80	0.76	39.9
All Ve		3976	2.0	0.910	37.6	LOS D	30.2	215.2	0.94	0.88	37.0

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

vement Performance - Pede	Demand	Average Delay		verage Back Pedestrian	of Queue Distance	Prop Queued	Effecti Stop R
Description	Flow ped/h	Delay	Bervice	ped	in		pelij
North Full Crossing	53	36.0	LOS D	0.1	0.1	0.92	0
West Full Crossing	53	33.3	LOS D	0.1	0.1	0.88	0

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Site: 12834 Whitmore St Fut AM

New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Mov	OD	rmance - V Demand		Deg.	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
ID	Mov	Total veh/h	HV %	Satn V/s	Delay sec	Service	Vehicles veh	Distance m	Oueued	Stop Rafe per ven	Speed km/h
South:	Customhou	se Quay									
1	L2	582	2.0	0.886	42.8	LOS D	28.8	205.1	1.00	0.93	34.6
2	T1	1083	2.0	0.664	30.0	LOS C	15.1	107.8	0.94	0.81	40.3
Appro	ach	1665	2.0	0.886	34.5	LOS C	28.8	205.1	0.96	0.85	38.1
East: \	NWL										
4	L2	14	0.0	0.165	48.2	LOS D	1.0	6.8	0.97	0.70	33.7
5	T1	19	0.0	0.165	42.7	LOS D	1.0	6.8	0.97	0.69	34.3
6	R2	12	0.0	0.165	48.2	LOS D	1.0	6.8	0.97	0.69	34.0
Appro	ach	44	0.0	0.165	45.8	LOS D	1.0	6.8	0.97	0.69	34.1
North:	Waterloo Qi	uay									
7	L2	105	2.0	0.889	42.5	LOS D	29.3	208.4	1.00	0.95	36.4
8	T1	1699	2.0	0.889	36.9	LOS D	29.5	209.7	1.00	0.95	37.3
9	R2	66	2.0	0.880	106.0	LOS F	6.1	43.7	1.00	0.92	21.7
Appro	ach	1871	2.0	0.889	39.7	LOS D	29.5	209.7	1.00	0.95	36.3
West:	Whitmore S										
10	L2	86	2.0	0.341	27.2	LOS C	7.3	52.2	0.77	0.75	41.3
11	 T1	53	2.0	0.341	21.6	LOS C	7.3	52.2	0.77	0.75	42.2
12	R2	312	2.0	0.341	27.3	LOS C	7.3	52.2	0.77	0.77	41.3
Appro		451	2.0	0.341	26.6	LOS C	7.3	52.2	0.77	0.76	41.4
All Ve	hiclas	4031	2.0	0,889	36,1	LOS D	29,5	209.7	0,96	0.88	37.

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Move Mov ID	nent Performance - Pedestri Description	Demand Flow ped/h	Average Delay sec	Level of Av Service P	erage Back o edestrian ped	of Queue Distance m	Prop Queued	Effective Stop Rate per ped
P3	North Full Crossing	53	32.8	LOS D	0.1	0.1	0.88	0.88
P4	West Full Crossing	53	34.4	LOS D	0.1	0.1	0.90	0.90

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

Processed: Monday, 15 September 2014 5:37:41 p.m. SIDRA INTERSECTION 6.0.24.4877
Project: G:\12834\SIDRA\Whitmore 2 way.sip6

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Mov	OD	rmance - V Demand	CONTRACTOR OF THE PROPERTY OF	Deg.	Average	Level of	95% Back		Prop.	Effective	Average
ID	Mov	Total veh/h	HV %	Saln Vic	Dalay sec	Service	Vehicles veh	Distance M	Queued	Stop Rate per veh	Speed km/h
South:	Customhou	se Quay									distilling of a
1	L2	525	2.0	0.866	41.0	LOS D	25.8	184.0	1.00	0.92	35.3
2	T1	1211	2.0	0.799	33.3	LOS C	18.1	129.2	0.99	0.88	38.9
Approa	ach	1736	2.0	0.866	35.6	LOS D	25.8	184.0	1.00	0.89	37.7
East: \	/ WL										
4	L2	48	0.0	0.454	47.3	LOS D	2.9	20.3	1.00	0.75	33.7
5	T1	40	0.0	0.454	41.7	LOS D	2.9	20.4	1.00	0.75	34.4
6	R2	40	0.0	0.454	47.3	LOS D	2.9	20.4	1.00	0.75	34.1
Appro	ach	128	0.0	0.454	45.6	LOS D	2.9	20.4	1.00	0.75	34.1
North:	Waterloo Q	uay									
7	L2	42	2.0	0.753	29.7	LOS C	18.8	134.0	0.94	0.83	41.9
8	T1	1512	2.0	0.753	23.8	LOSC	18.9	134.5	0.93	0.81	43.1
9	R2	108	2.0	0.861	95.6	LOS F	9.3	66.1	1.00	0.92	23.2
Appro	ach	1662	2.0	0.861	28.7	LOSC	18.9	134.5	0.93	0.82	40.8
West:	Whitmore S	t i i i i i i i i i i i i i i i i i i i									
10	L2	343	2.0	0.632	30.9	LOS C	15.0	106.5	0.90	0.83	39.3
11	T1	42	2.0	0.632	25.3	LOS C	15.0	106.5	0.90	0.83	40.1
12	R2	126	2.0	0.208	27.0	LOSC	4.1	29.4	0.76	0.74	41.3
Appro		512	2.0	0.632	29.5	LOSC	15.0	106.5	0.87	0.81	39.8
مرز الد	hicles	4038	1.9	0.866	32.3	LOS C	25,8	184.0	0.95	0.85	39.

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Novement Performance Nov D Description	Den F	iand ow	Average Delay		Average Back o Pedestrian ped	f Queue Distance m	Prop. Quetied S	Effective Hop Rat per pe
3 North Full Crossing	1 × 1	≘6//0 53	34.3	LOS D	0.1	0.1	0.92	0.9
24 West Full Crossing	-	53	34.8	LOS D	0.1	0.1	0.93	0.9

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Move	ment Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn V/o	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance In	Prop. Queuad	Effective Stop Rate per veh	Average Speed km/f
South:	Customhou	CHECK THE PROPERTY OF THE PROP									
1	L2	506	2.0	0.871	43.4	LOS D	24.7	176.1	1.00	0.92	34.5
2	T1	1576	2.0	0.910	46.3	LOS D	30.2	215.2	1.00	0.99	34.2
Appro	ach	2082	2.0	0.910	45.6	LOS D	30.2	215.2	1.00	0.97	34.2
East: \	MWL										
4	L2	40	0.0	0.305	49.0	LOS D	1.8	12.6	0.98	0.73	32.7
5	T1	17	0.0	0.203	42.9	LOS D	1.2	8,5	0.97	0.70	34.6
6	R2	11	0.0	0.203	48.5	LOS D	1.2	8.5	0.97	0.70	34.2
Appro	ach	67	0.0	0.305	47.4	LOS D	1.8	12.6	0.98	0.72	33.4
North:	Waterloo Q	uay		13034.000							
7	L2	52	2.0	0.667	28.2	LOS C	17.9	127.1	0.88	0.78	42.6
8	T 1	1448	2.0	0.667	22.4	LOS C	17.9	127.7	0.87	0.77	43.8
9	R2	105	2.0	0.888	103.8	LOS F	9.7	69.1	1.00	0.94	22.0
Appro	ach	1605	2.0	0.888	27.9	LOS C	17.9	127.7	0.88	0.78	41.1
West:	Whitmore S										
10	L2	185	2.0	0.336	29.7	LOS C	6.7	47.6	0.81	0.78	39.7
11	T1	11	2.0	0.336	24.2	LOS C	6.7	47.6	0.81	0.78	40.
12	R2	25	2.0	0.043	27.2	LOS C	0.8	5.5	0.72	0.68	41.1
Appro	ach	221	2.0	0.336	29.2	LOSC	6.7	47.6	0.80	0.76	39.9
All Ve	hicles	3976	2,0	0.910	37,6	LOS D	30.2	215,2	0,94	0.88	37.0

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

lovi	Performance - Pedestria	Demand	Average	Level of A	verage Back (of Queue	Prop.	Effective
n Des	renjetion	Flow	Delay	Service	Pedestrian	Distance	Quetted	Stop Rai
		ped/h	Sec		ped	m	A SECTION OF THE SECTION	[p=); [0=
3 Nor	th Full Crossing	53	36.0	LOS D	0.1	0.1	0.92	0.9
•	st Full Crossing	53	33.3	LOS D	0.1	0.1	0.88	3,0

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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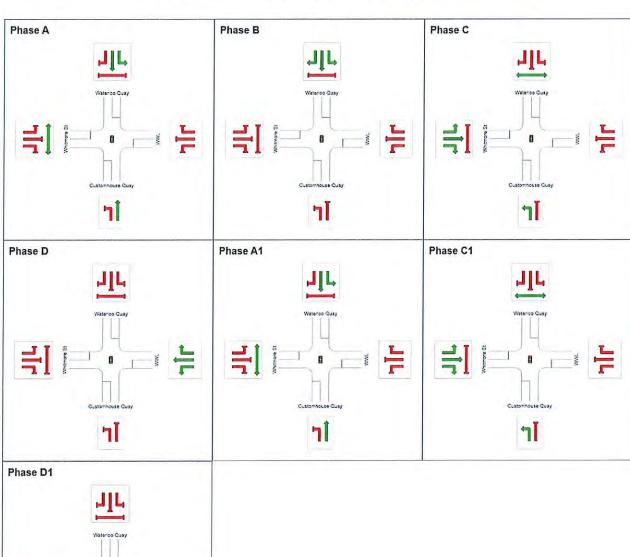
Site: 12834 Whitmore St Ex AM

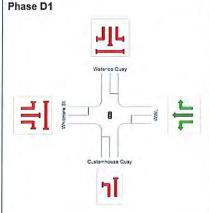
New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS
Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	40	78	90	123	158
Green Time (sec)	21	7	32	6	27	29	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	13	38	12	33	35	12
Phase Split	16 %	8 %	22 %	7 %	19 %	21 %	7 %





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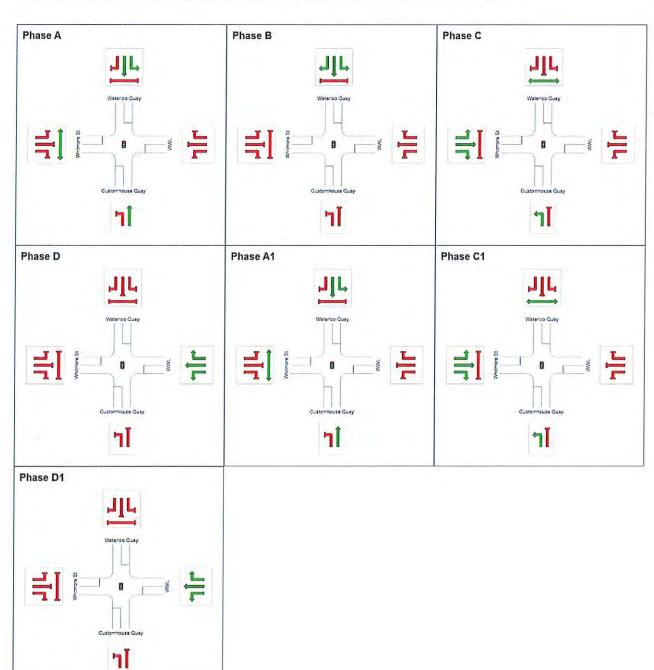
New Site

Signals - Fixed Time Cycle Time = 160 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS

Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	77	89	116	148
Green Time (sec)	21	11	27	6	21	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	33	12	27	32	12
Phase Split	17 %	11 %	21 %	8 %	17 %	20 %	8 %



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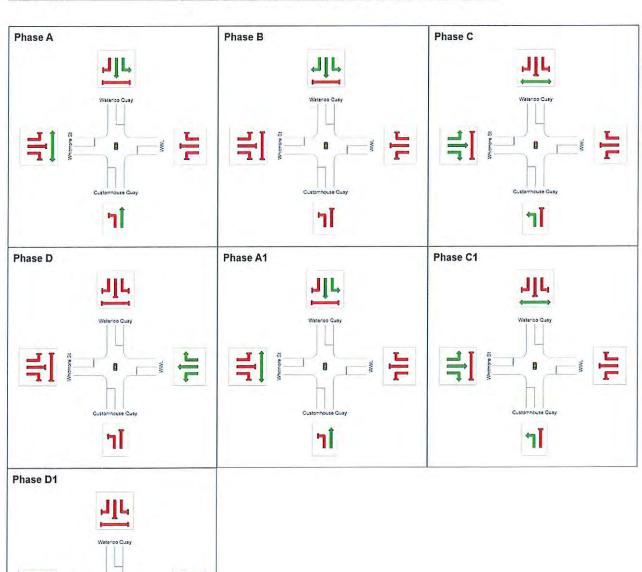
New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS
Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

זר

Phase	Α	В	С	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	78	90	126	158
Green Time (sec)	21	11	28	6	30	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	34	12	36	32	12
Phase Split	16 %	10 %	20 %	7 %	21 %	19 %	7 %





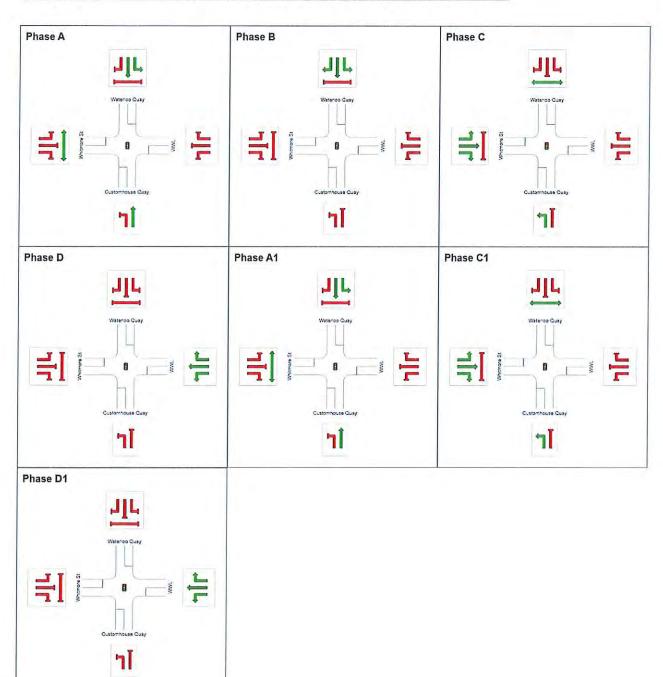
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New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	A	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	40	78	90	123	158
Green Time (sec)	21	7	32	6	27	29	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	13	38	12	33	35	12
Phase Split	16 %	8 %	22 %	7 %	19 %	21 %	7 %





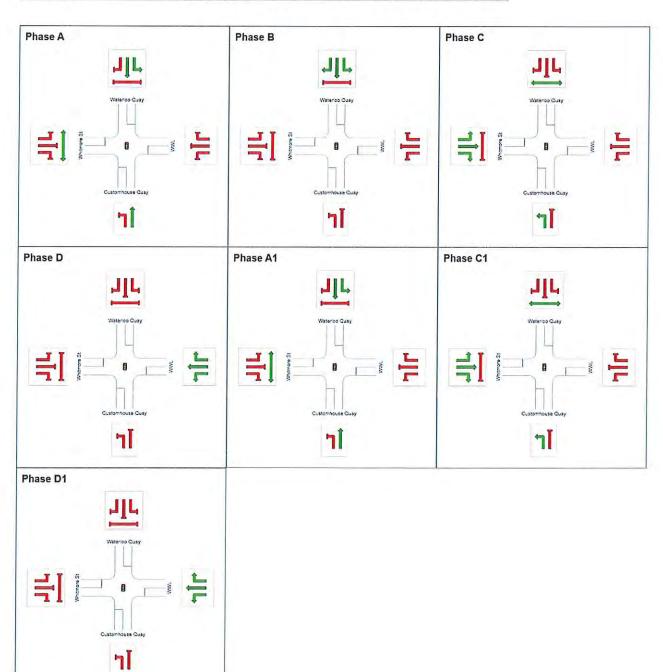
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New Site

Signals - Fixed Time Cycle Time = 160 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	77	89	116	148
Green Time (sec)	21	11	27	6	21	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	33	12	27	32	12
Phase Split	17 %	11 %	21 %	8 %	17 %	20 %	8 %





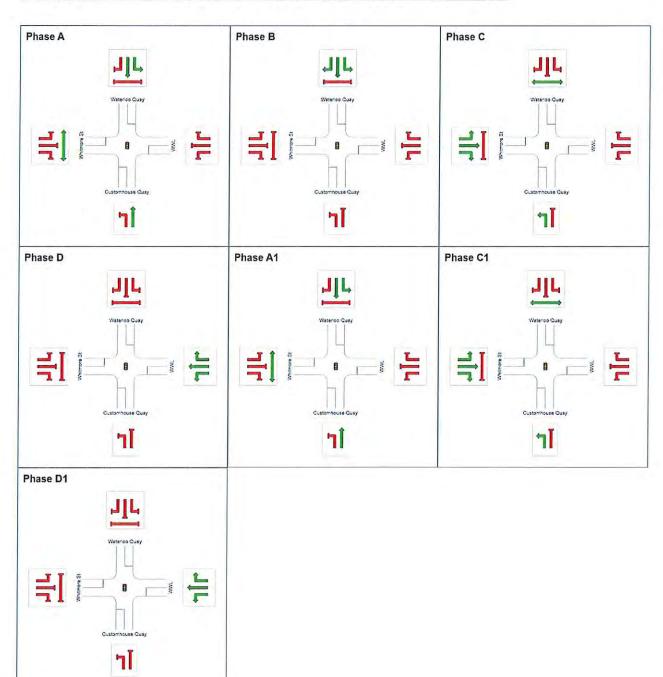
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New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	78	90	126	158
Green Time (sec)	21	11	28	6	30	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	34	12	36	32	12
Phase Split	16 %	10 %	20 %	7 %	21 %	19 %	7 %



Appendix D2

Data Responding to Item 14 (One-Way Lane Configuration)

Site: 12834 Whitmore St Ex AM

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Mov	OD	Demand	Flows	Deg.	Average	Level of	95% Back (Prop	Effective	Average
ID)	Mov	Total	HV %	Sath	Delay	Service	Vehicles veh	Distance m	Quetied	Stop Rate per veh	Speed km/l
South:	Customhou	veh/h se Quav	year and the second	V/c	Sé¢						
1	L2	582	2.0	0.886	42.8	LOS D	28.8	205.1	1.00	0.93	34.0
2	T1	1083	2.0	0.664	30.0	LOS C	15.1	107.8	0.94	0.81	40.
Appro	ach	1665	2.0	0.886	34.5	LOS C	28.8	205.1	0.96	0.85	38.
East: \	∕WL										4.400.000
4	L2	14	0.0	0.081	47.6	LOS D	0.5	3.3	0.96	0.67	33.
5	T1	19	0.0	0.081	42.0	LOS D	0.5	3,4	0.96	0.65	35.4
6	R2	12	0.0	0.088	47.7	LOS D	0.5	3.5	0.96	0.67	33.
Appro	ach	44	0.0	0.088	45.2	LOS D	0.5	3.5	0.96	0,66	34.
North:	Waterloo Qu	uay									
7	L2	105	2.0	0.889	42.5	LOS D	29.3	208.4	1.00	0.95	36.
8	T1	1699	2.0	0.889	36.9	LOS D	29.5	209.7	1.00	0.95	37.
9	R2	66	2.0	0.880	106.0	LOS F	6.1	43.7	1.00	0.92	21.
Appro	ach	1871	2.0	0.889	39.7	LOS D	29.5	209.7	1.00	0.95	36.
West:	Whitmore S										
10	L2	86	2.0	0.341	27.2	LOS C	7.3	52.2	0,77	0.75	41.
11	T1	53	2.0	0.341	21.6	LOS C	7.3	52.2	0.77	0.75	42.
12	R2	312	2.0	0.341	27.3	LOS C	7.3	52.2	0.77	0.77	41.
Аррго	ach	451	2.0	0.341	26.6	LOS C	7.3	52.2	0.77	0.76	41.
110000	hicles	4031	2.0	0.889	36.1	LOS D	29.5	209.7	0.96	0.88	37,

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Move Mov JD	ment Performance - Pedestria Description	ns Demand Flow ped/h	Average Delay	Level of Service	Average Back o Padestrian ped	of Queue Distance m	Prop. Queued	Effective Stop Rate per ped
P3	North Full Crossing	53	32.8	LOS D	0.1	0.1	0.88	0.88
P4	West Full Crossing	53	34.4	LOS D	0.1	0.1	0.90	0.90
All Pe	destrians	105	33.6	LOS D			0.89	0.89

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Signals - Fixed Time Cycle Time = 160 seconds (Practical Cycle Time)

Mov	OD	Demand		Deg.	Average	Level of	95% Back		Prop.	Effective	Averag
ID)	Mov	Total veh/h	HV %	Saln V/c	Delay sec	Service	Vehicles veh	Distance m	Queued	Stop Rate per veh	Speed km/
South	: Customhou										
1	L2	525	2.0	0.866	41.0	LOS D	25.8	184.0	1.00	0.92	35.
2	T1	1211	2.0	0.799	33.3	LOS C	18.1	129.2	0.99	0.88	38.
Appro	ach	1736	2.0	0.866	35.6	LOS D	25.8	184.0	1.00	0.89	37.
East:	WWL				Altanience Wither						
4	L2	48	0.0	0.207	46.1	LOS D	1.3	9.0	0.97	0.71	33.
5	T1	40	0.0	0.207	40.5	LOS D	1.3	9.3	0.97	0.70	35.
6	R2	40	0.0	0.287	46.6	LOS D	1.8	12.4	0.98	0.73	33.
Appro	ach	128	0.0	0.287	44.5	LOS D	1.8	12.4	0.97	0.71	34.
North	Waterloo Q	uay							6 () = 0 () 6 () may 6 () 1 ()		
7	L2	42	2.0	0.753	29.7	LOSC	18.8	134.0	0.94	0.83	41.
8	T1	1512	2.0	0.753	23.8	LOS C	18.9	134.5	0.93	0.81	43.
9	R2	108	2.0	0.861	95.6	LOS F	9.3	66.1	1.00	0.92	23.
Appro	ach	1662	2.0	0.861	28.7	LOS C	18.9	134.5	0.93	0.82	40.
West:	Whitmore S	t arahan kan						Zu sanasti.			Any views:
10	L2	343	2.0	0.632	30.9	LOSC	15.0	106.5	0.90	0.83	39
11	T1	42	2.0	0.632	25.3	LOS C	15.0	106.5	0.90	0.83	40
12	R2	126	2.0	0.208	27.0	LOS C	4.1	29.4	0.76	0.74	41
Appro	ach	512	2.0	0.632	29.5	LOS C	15.0	106.5	0.87	0.81	39.
Λ II \	hicles	4038	1.9	0.866	32.3	LOS C	25.8	184.0	0.95	0.85	39

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Mov	ment Performance - Pedestr Description	Demand Flow	Average Delav		erage Back of ledestrian	Queue Distance	Prop. Queued	JEffectiv Stop Ra
U		ped/h	8é¢		presel	m	0.00]ଶ୍ୟାଣ୍ଡ 0.9
93	North Full Crossing	53	34.3	LOS D	0.1	0.1	0.92 0.93	0.9
74	West Full Crossing	53	34.8	LOS D	U.1	U, 1 777-11: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1:		UERIA E E E

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Mov	ØĐ	Demand	Flows	Deg.	Average	Level of	95% Back		Prop	Effective	Average
ID	Mov	Total veh/h	HV %	Satn V/c	Delay sec	Service	Vehicles veh	Distance m	Queued	Stop Rate per veh	Speed km/h
South:	Customhou	A SECULIAR S									
1	L2	506	2.0	0.871	43.4	LOS D	24.7	176.1	1.00	0.92	34.5
2	T 1	1576	2.0	0.910	46.3	LOS D	30.2	215.2	1.00	0.99	34.2
Approa	ach	2082	2.0	0.910	45.6	LOS D	30.2	215.2	1.00	0.97	34.2
East; V	VVVL										
4	L2	40	0.0	0.153	48.2	LOS D	0.9	6.2	0.97	0.70	33.0
5	T1	17	0.0	0.122	42.3	LOS D	0.7	5.2	0.97	0.67	35.6
6	R2	11	0.0	0.080	47.7	LOS D	0.5	3.2	0.96	0.67	33.3
Appro	ach	67	0.0	0.153	46.6	LOS D	0.9	6.2	0.97	0.69	33.7
North:	Waterloo Q	uay		ÇIYERININ P		7-18 19-10 19-10 17-17-18-18					
7	L2	52	2.0	0.667	28.2	LOS C	17.9	127.1	0.88	0.78	42.6
8	T1	1448	2.0	0.667	22.4	LOSC	17.9	127.7	0.87	0.77	43.8
9	R2	105	2.0	0.888	103.8	LOS F	9.7	69.1	1.00	0.94	22.0
Appro	ach	1605	2.0	888.0	27.9	LOS C	17.9	127.7	0.88	0.78	41.1
West:	Whitmore S	t in the second									
10	L2	185	2.0	0.336	29.7	LOS C	6.7	47.6	0.81	0.78	39.7
11	Т1	11	2.0	0.336	24.2	LOS C	6.7	47.6	0.81	0.78	40.
12	R2	25	2.0	0.043	27.2	LOS C	8,0	5.5	0.72	0.68	41.1
Appro	ach	221	2.0	0.336	29.2	LOSC	6.7	47.6	0.80	0.76	39.9
All Ve	hiolog	3976	2.0	0,910	37.6	LOS D	30.2	215.2	0.94	0.88	37.0

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

vement Performance - Pede	Demand	Average Delay		verage Back Pedestrian	of Queue Distance	Prop Queued	Effecti Stop R
Description	Flow ped/h	Delay	Bervice	ped	in		pelij
North Full Crossing	53	36.0	LOS D	0.1	0.1	0.92	0
West Full Crossing	53	33.3	LOS D	0.1	0.1	0.88	0

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Mov	OD	rmance - V Demand		Deg.	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
ID	Mov	Total veh/h	HV %	Satn V/s	Delay sec	Service	Vehicles veh	Distance m	Oueued	Stop Rafe per ven	Speed km/h
South:	Customhou	se Quay									
1	L2	582	2.0	0.886	42.8	LOS D	28.8	205.1	1.00	0.93	34.6
2	T1	1083	2.0	0.664	30.0	LOS C	15.1	107.8	0.94	0.81	40.3
Appro	ach	1665	2.0	0.886	34.5	LOS C	28.8	205.1	0.96	0.85	38.1
East: \	NWL										
4	L2	14	0.0	0.165	48.2	LOS D	1.0	6.8	0.97	0.70	33.7
5	T1	19	0.0	0.165	42.7	LOS D	1.0	6.8	0.97	0.69	34.3
6	R2	12	0.0	0.165	48.2	LOS D	1.0	6.8	0.97	0.69	34.0
Appro	ach	44	0.0	0.165	45.8	LOS D	1.0	6.8	0.97	0.69	34.1
North:	Waterloo Qi	uay									
7	L2	105	2.0	0.889	42.5	LOS D	29.3	208.4	1.00	0.95	36.4
8	T1	1699	2.0	0.889	36.9	LOS D	29.5	209.7	1.00	0.95	37.3
9	R2	66	2.0	0.880	106.0	LOS F	6.1	43.7	1.00	0.92	21.7
Appro	ach	1871	2.0	0.889	39.7	LOS D	29.5	209.7	1.00	0.95	36.3
West:	Whitmore S										
10	L2	86	2.0	0.341	27.2	LOS C	7.3	52.2	0.77	0.75	41.3
11	 T1	53	2.0	0.341	21.6	LOS C	7.3	52.2	0.77	0.75	42.2
12	R2	312	2.0	0.341	27.3	LOS C	7.3	52.2	0.77	0.77	41.3
Appro		451	2.0	0.341	26.6	LOS C	7.3	52.2	0.77	0.76	41.4
All Ve	hiclas	4031	2.0	0,889	36,1	LOS D	29,5	209.7	0,96	0.88	37.

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Move Mov ID	nent Performance - Pedestri Description	Demand Flow ped/h	Average Delay sec	Level of Av Service P	erage Back o edestrian ped	of Queue Distance m	Prop Queued	Effective Stop Rate per ped
P3	North Full Crossing	53	32.8	LOS D	0.1	0.1	0.88	0.88
P4	West Full Crossing	53	34.4	LOS D	0.1	0.1	0.90	0.90

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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New Site

Mov	OD	rmance - V Demand	CONTRACTOR OF THE PROPERTY OF	Deg	Average	Level of	95% Back		Prop.	Effective	Average
ID	Mov	Total veh/h	HV %	Saln Ws	Dalay sec	Service	Vehicles veh	Distance M	Queued	Stop Rate per veh	Speed km/h
South:	Customhou	se Quay			1 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1						distilling of a
1	L2	525	2.0	0.866	41.0	LOS D	25.8	184.0	1.00	0.92	35.3
2	T1	1211	2.0	0.799	33.3	LOS C	18.1	129.2	0.99	0.88	38.9
Approa	ach	1736	2.0	0.866	35.6	LOS D	25.8	184.0	1.00	0.89	37.7
East: V	/ WL										
4	L2	48	0.0	0.454	47.3	LOS D	2.9	20.3	1.00	0.75	33.7
5	T1	40	0.0	0.454	41.7	LOS D	2.9	20.4	1.00	0.75	34.4
6	R2	40	0.0	0.454	47.3	LOS D	2.9	20.4	1.00	0.75	34.1
Appro	ach	128	0.0	0.454	45.6	LOS D	2.9	20.4	1.00	0.75	34.1
North:	Waterloo Q	uay									
7	L2	42	2.0	0.753	29.7	LOS C	18.8	134.0	0.94	0.83	41.9
8	T1	1512	2.0	0.753	23.8	LOSC	18.9	134.5	0.93	0.81	43.1
9	R2	108	2.0	0.861	95.6	LOS F	9.3	66.1	1.00	0.92	23.2
Appro	ach	1662	2.0	0.861	28.7	LOSC	18.9	134.5	0.93	0.82	40.8
West:	Whitmore S	t i i i i i i i i i i i i i i i i i i i									
10	L2	343	2.0	0.632	30.9	LOSC	15.0	106.5	0.90	0.83	39.3
11	T1	42	2.0	0.632	25.3	LOS C	15.0	106.5	0.90	0.83	40.1
12	R2	126	2.0	0.208	27.0	LOSC	4.1	29.4	0.76	0.74	41.3
Appro		512	2.0	0.632	29.5	LOS C	15.0	106.5	0.87	0.81	39.8
مرا الم	hicles	4038	1.9	0.866	32.3	LOS C	25,8	184.0	0.95	0.85	39.

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

lovement Performance lov D Description	Den F	iand ow	Average Delay		Average Back o Pedestrian ped	f Queue Distance m	Prop. Quetied \$	Effective Itop Rat per pe
3 North Full Crossing	1 × 1	≘6//0 53	34.3	LOS D	0.1	0.1	0.92	0.9
4 West Full Crossing	-	53	34.8	LOS D	0.1	0.1	0.93	9.0

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Move	ment Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn V/o	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance In	Prop. Queuad	Effective Stop Rate per veh	Average Speed km/f
South:	Customhou	CHECK THE PROPERTY OF THE PROP									
1	L2	506	2.0	0.871	43.4	LOS D	24.7	176.1	1.00	0.92	34.5
2	T1	1576	2.0	0.910	46.3	LOS D	30.2	215.2	1.00	0.99	34.2
Appro	ach	2082	2.0	0.910	45.6	LOS D	30.2	215.2	1.00	0.97	34.2
East: \	MWL										
4	L2	40	0.0	0.305	49.0	LOS D	1.8	12.6	0.98	0.73	32.7
5	T1	17	0.0	0.203	42.9	LOS D	1.2	8,5	0.97	0.70	34.6
6	R2	11	0.0	0.203	48.5	LOS D	1.2	8.5	0.97	0.70	34.2
Appro	ach	67	0.0	0.305	47.4	LOS D	1.8	12.6	0.98	0.72	33.4
North:	Waterloo Q	uay		13034.000							
7	L2	52	2.0	0.667	28.2	LOS C	17.9	127.1	0.88	0.78	42.6
8	T 1	1448	2.0	0.667	22.4	LOS C	17.9	127.7	0.87	0.77	43.8
9	R2	105	2.0	0.888	103.8	LOS F	9.7	69.1	1.00	0.94	22.0
Appro	ach	1605	2.0	0.888	27.9	LOS C	17.9	127.7	0.88	0.78	41.1
West:	Whitmore S										
10	L2	185	2.0	0.336	29.7	LOS C	6.7	47.6	0.81	0.78	39.7
11	T1	11	2.0	0.336	24.2	LOS C	6.7	47.6	0.81	0.78	40.
12	R2	25	2.0	0.043	27.2	LOS C	0.8	5.5	0.72	0.68	41.1
Appro	ach	221	2.0	0.336	29.2	LOSC	6.7	47.6	0.80	0.76	39.9
All Ve	hicles	3976	2,0	0.910	37,6	LOS D	30.2	215,2	0,94	0.88	37.0

Level of Service (LOS) Method: Delay (HCM 2000).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

A.	nance - Pedestria	Demand	Average	Level of A	verage Back	of Queue	Prop	Effective
Description		FloW	Delay	Service	Pedestrian	Distance	Quetted	Stop Rai
		ped/h	Sec		lateig .	m		per pe
3 North Full Cr	ossina	53	36.0	LOS D	0.1	0.1	0.92	0.9
4 West Full Cr	•	53	33.3	LO\$ D	0.1	0.1	0.88	0.8

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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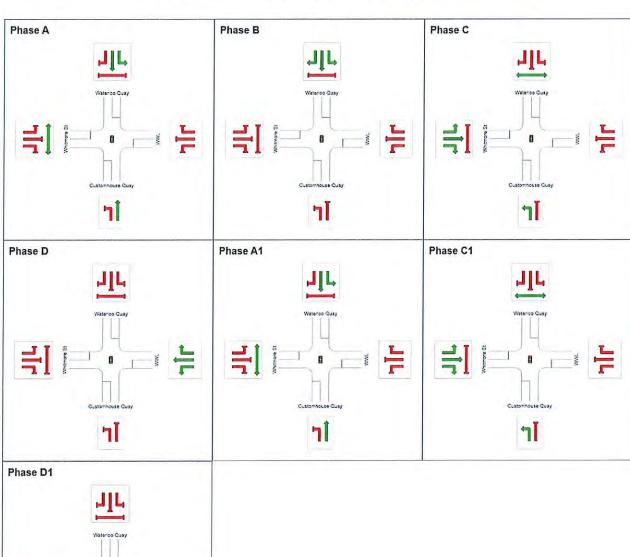
Site: 12834 Whitmore St Ex AM

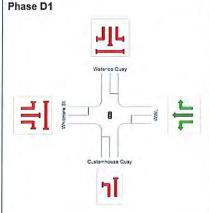
New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS
Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	40	78	90	123	158
Green Time (sec)	21	7	32	6	27	29	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	13	38	12	33	35	12
Phase Split	16 %	8 %	22 %	7 %	19 %	21 %	7 %





Site: 12834 Whitmore St Ex PM

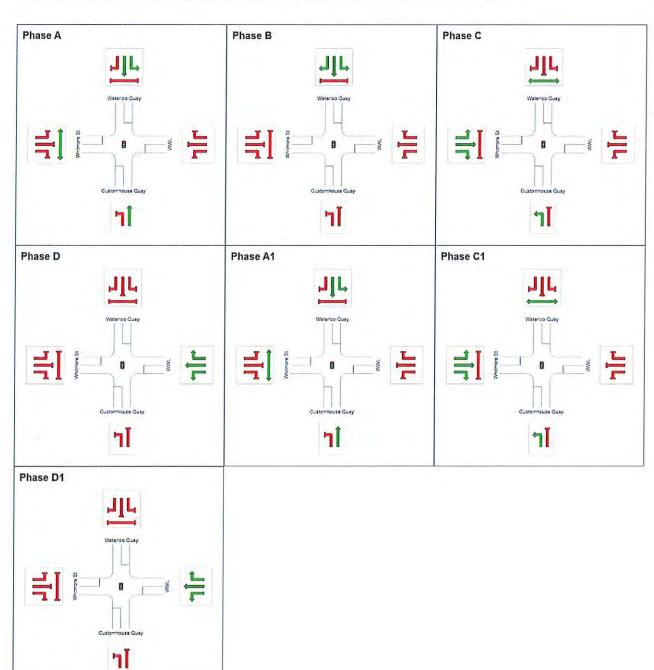
New Site

Signals - Fixed Time Cycle Time = 160 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS

Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	77	89	116	148
Green Time (sec)	21	11	27	6	21	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	33	12	27	32	12
Phase Split	17 %	11 %	21 %	8 %	17 %	20 %	8 %



Site: 12834 Whitmore St Ex Sat

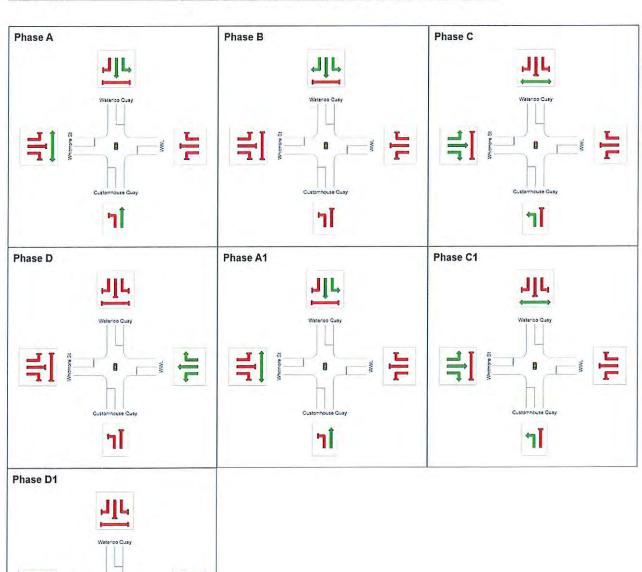
New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS
Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

זר

Phase	Α	В	С	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	78	90	126	158
Green Time (sec)	21	11	28	6	30	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	34	12	36	32	12
Phase Split	16 %	10 %	20 %	7 %	21 %	19 %	7 %





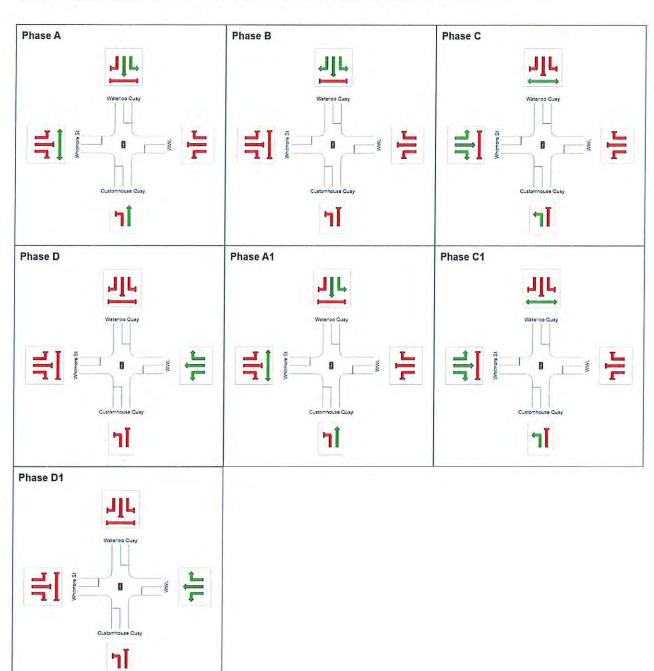
Site: 12834 Whitmore St Fut AM

New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	A	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	40	78	90	123	158
Green Time (sec)	21	7	32	6	27	29	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	13	38	12	33	35	12
Phase Split	16 %	8 %	22 %	7 %	19 %	21 %	7 %





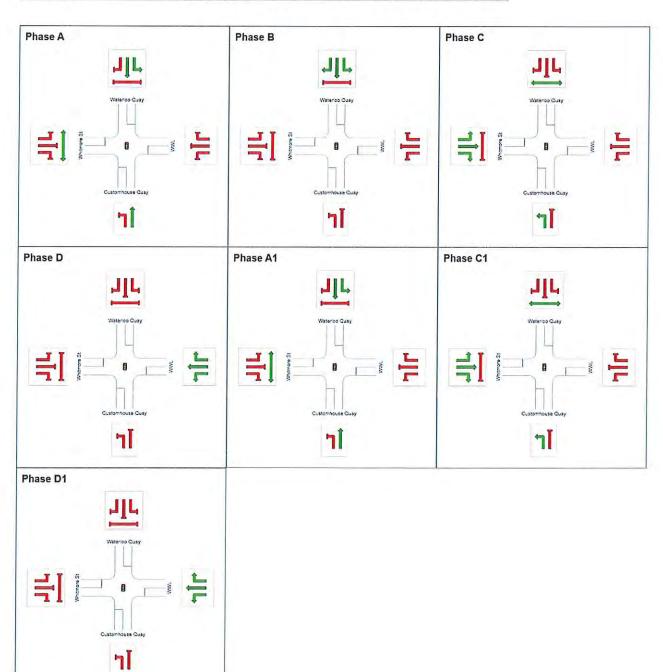
Site: 12834 Whitmore St Fut PM

New Site

Signals - Fixed Time Cycle Time = 160 seconds (Practical Cycle Time)

Phase times determined by the program Sequence: SCATS Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	77	89	116	148
Green Time (sec)	21	11	27	6	21	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	33	12	27	32	12
Phase Split	17 %	11 %	21 %	8 %	17 %	20 %	8 %





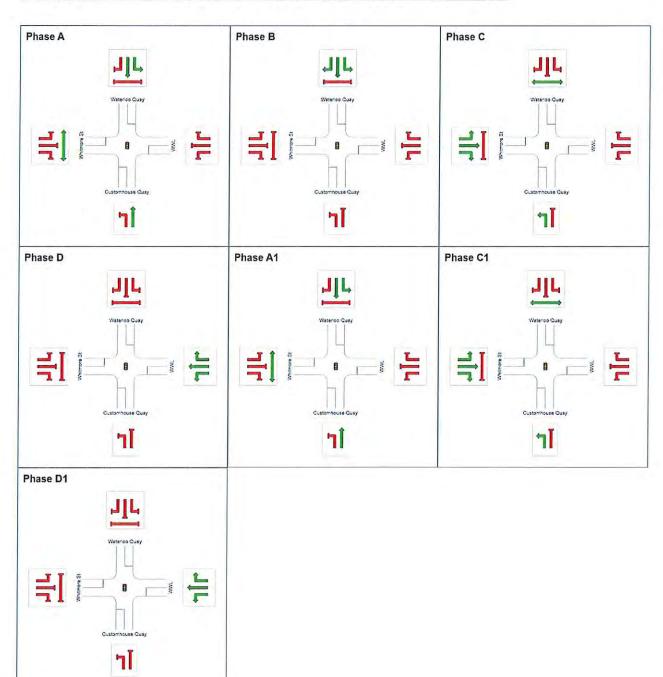
Site: 12834 Whitmore St Fut Sat

New Site

Signals - Fixed Time Cycle Time = 170 seconds (Practical Cycle Time)

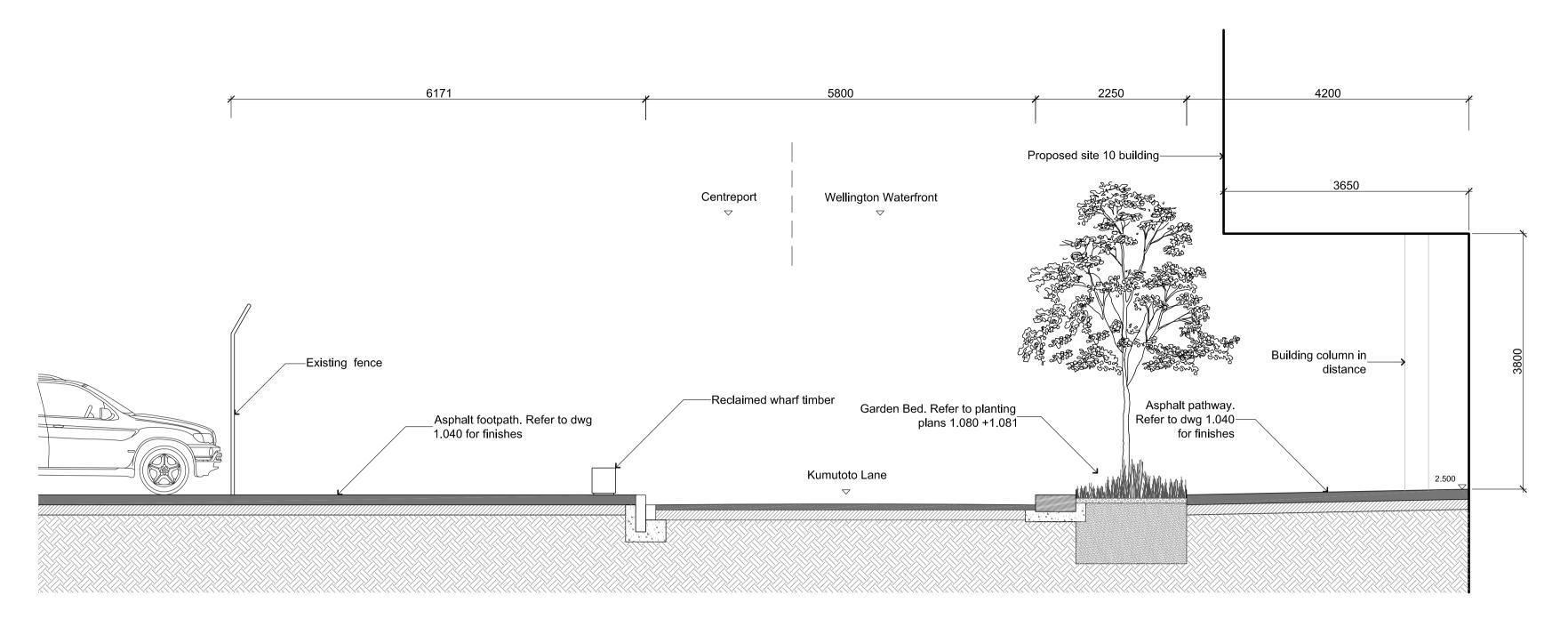
Phase times determined by the program Sequence: SCATS Movement Class: All Movement Classes Input Sequence: A, B, C, D, A1, C1, D1 Output Sequence: A, B, C, D, A1, C1, D1

Phase	Α	В	C	D	A1	C1	D1
Reference Phase	Yes	No	No	No	No	No	No
Phase Change Time (sec)	0	27	44	78	90	126	158
Green Time (sec)	21	11	28	6	30	26	6
Yellow Time (sec)	4	4	4	4	4	4	4
All-Red Time (sec)	2	2	2	2	2	2	2
Phase Time (sec)	27	17	34	12	36	32	12
Phase Split	16 %	10 %	20 %	7 %	21 %	19 %	7 %

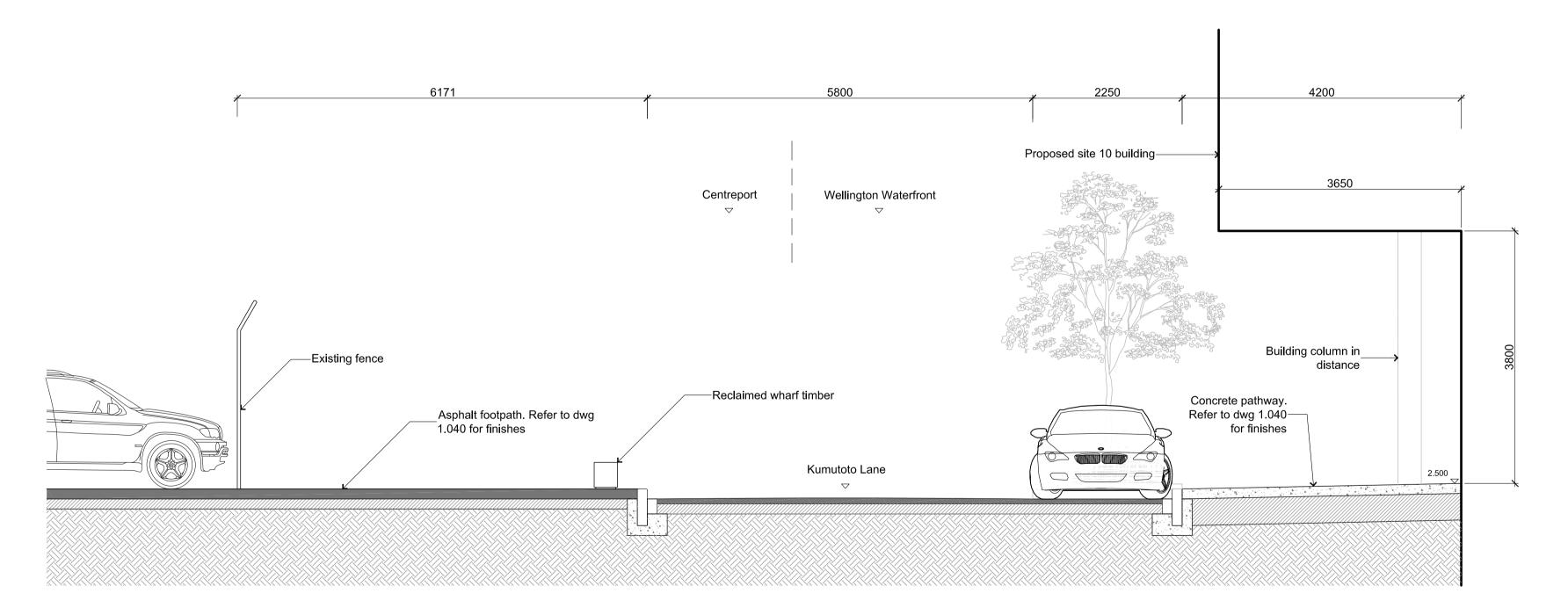


Appendix E

Plan Responding to Item 15



Kumutoto Laneway Section
Scale: 1:50@ A1 | 1:100@A3

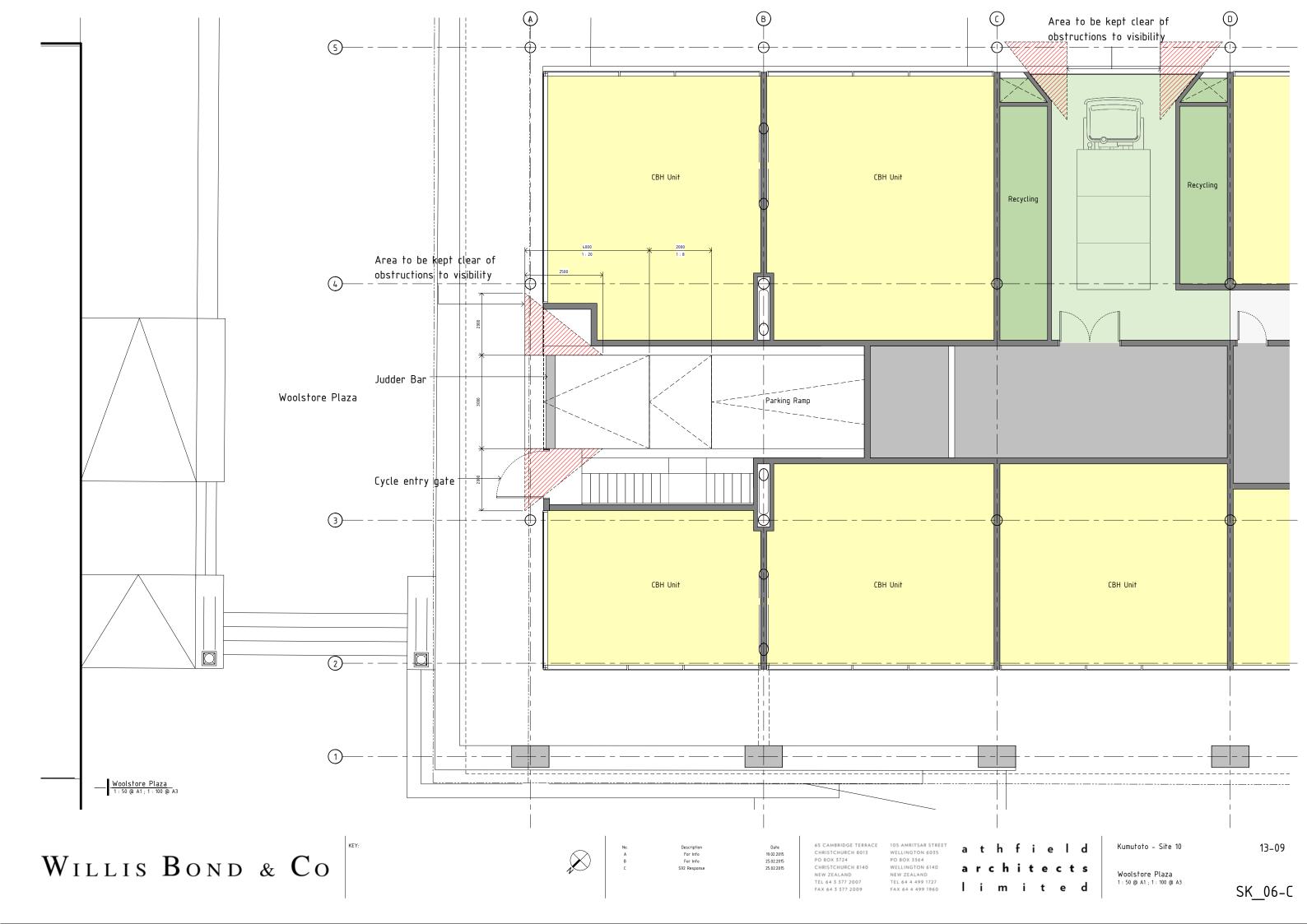


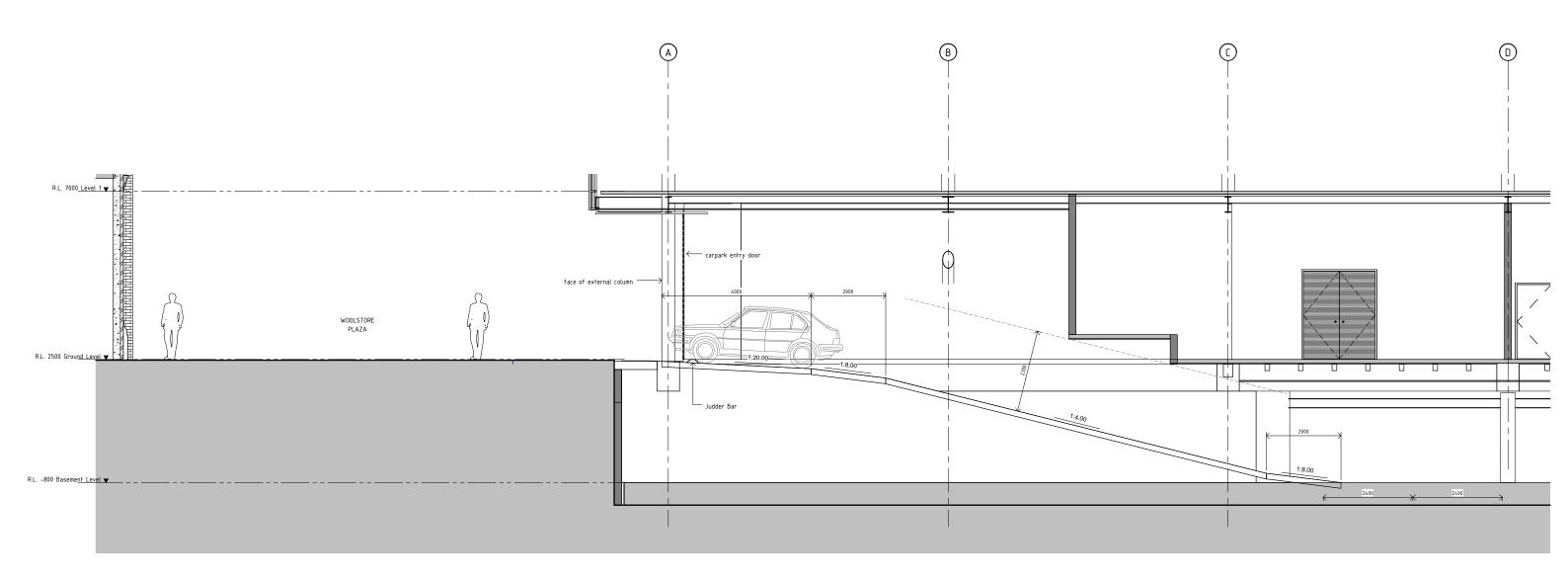
Kumutoto Laneway Section
Scale: 1:50@ A1 | 1:100@A3



Appendix F

Plans Responding to Item 17





_______Carpark Ramp 1:50 @ A1;1:100 @ A3

Willis Bond & Co

 No.
 Description

 A
 For Info

 B
 For Info

 C
 For Info

 D
 S92 Response

Date 65 C 16.02.2015 CHR 19.02.2015 PO E 25.02.2015 CHR 25.02.2015 NEW

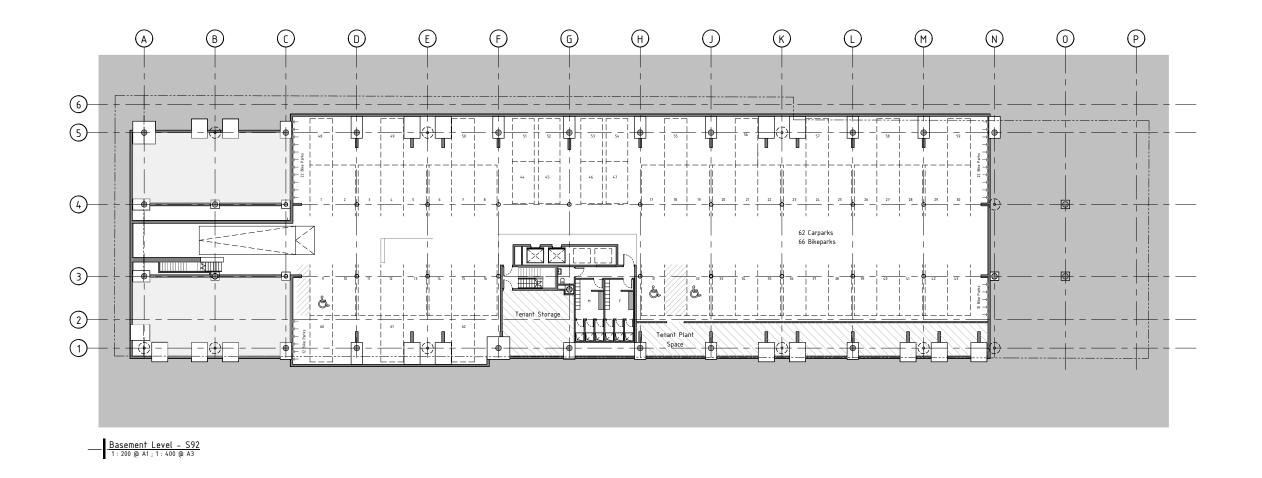
65 CAMBRIDGE TERRACE
CHRISTCHURCH 8013
PO BOX 3724
CHRISTCHURCH 8140
NEW ZEALAND
TEL 64 3 377 2007
FAX 64 4 499 1727
FAX 64 4 499 1960

Kumutoto - Site 10

Carpark Ramp 1:50 @ A1;1:100 @ A3

SK_05-D

13-09



STRUCTURAL ENGINEER:
NAME : Dunning Thornton Consultants Ltd
PH
FAX
PO BOX
EMAIL

SERVICES ENGINEER: NAME : AECOM PH FAX PO BOX EMAIL

FIRE ENGINEER: NAME: Holmes Fire PH FAX PO BOX EMAIL KEY:



Description
FOR DISCUSSION
Tenant Review
Tenant Review update
S92 Response

Date 26.09.2014 01.12.2014 09.12.2014 25.02.2015 65 CAMBRIDGE TERRACE CHRISTCHURCH 8013 WELLINGTON 6035 PO BOX 5724 PO BOX 3564 WELINGTON 6140 NEW ZEALAND NEW ZEALAND TEL 64 3 377 2007 FAX 64 4 499 1960

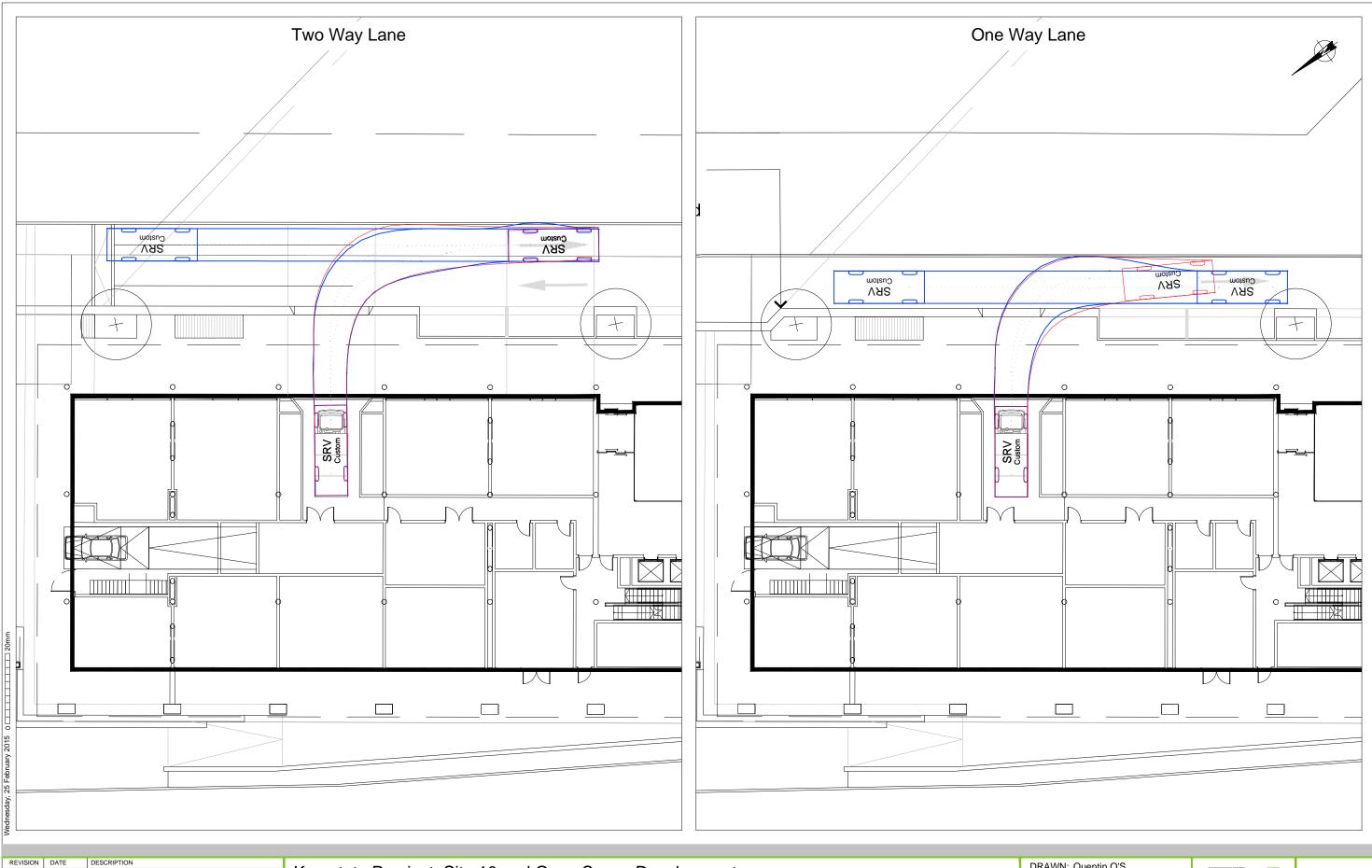
105 AMRITSAR STREET WELLINGTON 6035 PO BOX 53644 WELLINGTON 6140 NEW ZEALAND TEL 64.4 499 1227 FAX 64.4 499 1960 A the street of the street of

Kumutoto - Site 10

Basement Plan 1: 200 @ A1; 1: 400 @ A3 @ A1 13-09

Appendix G

Plan Responding to Item 22



Kumutoto Precinct: Site 10 and Open Space Development Loading Bay Manoeuvres DRAWN: Quentin O'S
DATE: 18/02/2015
SCALE: 1:250 @ A3

DWG NO:12834W1A

TDG

7a